



Phase noise mitigation by a realistic optical parametric oscillator

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We address the exploitation of an optical parametric oscillator (OPO) in the task of mitigating, at least partially, phase noise produced by phase diffusion. In particular, we analyze two scenarios where phase diffusion is typically present. The first one is the measurement of the phase of a noisy optical field, while the second involves a quantum estimation scheme of a phase shift imposed on a noisy probe. In both cases, we prove that an OPO may lead to a partial or full compensation of the noise. © 2022 Optical Society of America

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1. INTRODUCTION

The phase of an optical field is a fundamental degree of freedom for several applications in quantum sensing and quantum communication. Quantum interferometry is exploited in high-precision measurements to detect fine perturbations through phase shifts [1–3] and continuous-variable communication protocols are often based on *phase shift keying* (PSK) [4–6]. However, the optical phase cannot be described as observable in a strict sense [7–10], and this result makes it challenging to provide a detailed description of all the strategies involving the phase.

In practical contexts, the phase of a field is often affected by phase noise, especially due to phase diffusion. Indeed, the presence of phase diffusion may lead to a partial or complete loss of all the advantages of quantum measurements. In the quantum optics scenario, phase diffusion efficiently describes the noisy propagation of quantum light through optical fibers [11], and its effect has been thoroughly investigated on phase estimation and quantum communication protocols [12–19]. More generally, its detrimental effects have been also investigated for different physical platforms, such as Bose–Einstein condensates [20,21] and Bose–Josephson junctions [22].

Focusing our attention on quantum optical systems, one of the possible resources to counteract phase noise is provided by a phase-sensitive amplifier, such as an *optical parametric oscillator* (OPO). More precisely, an OPO is not expected to be useful to improve measurements, i.e., to build receivers, because the induced phase shift would lead to a modification of the phase outcome. On the contrary, an OPO may be very effective in order to improve the properties of the probe state if affected by phase noise.

In this work, we address the possibility of using an OPO to compensate, at least partially, the detriments of phase noise. In particular, we present a theoretical model approaching the task of removing phase noise of a laser. Our method could be effective to reduce the laser phase noise at high frequency (between 100 kHz and 10 MHz). At these frequencies, it is hard to distinguish between amplitude and phase noise to act on the phase noise, but our technique acts directly on the phase, and it is not influenced by the amplitude noise. Hints that squeezing could help in this scenario have already been shown in [23,24]. Here, we discuss in more detail a realistic experimental implementation of a squeezing operation via an OPO, taking into account the most relevant experimental details. Moreover, we apply the scenario described above to two different cases where the optical phase is exploited. The first one is a pure *quantum optical* context and regards the measurement of the phase of a quantum state of radiation. On the contrary, the second case consists of a *quantum estimation* scheme, where information is encoded on a phase shift. In both cases, we consider single mode radiation prepared in a coherent state $|\alpha\rangle$, $\alpha \in \mathbb{R}_+$ undergoing phase diffusion. Just after dephasing, we introduce an OPO and discuss if its exploitation may lead to noise mitigation.

The paper is structured as follows. First of all, in Section 2, we present a theoretical model for the OPO, described in the Schrödinger picture, allowing us to work directly at the level of quantum states. Bearing that in mind, we apply it to the two cases examined. In Section 3, we address the measurement of an optical phase and state, in which the conditions the OPO are able to counteract phase noise, while Section 4 is dedicated to describing the estimation scheme with the tools of quantum estimation theory and to find out the optimal measurement to detect the value of the encoded phase shift with the highest

possible precision. We close our investigation drawing some concluding remarks in Section 5.

2. BLOCK-DIAGRAM MODEL FOR THE OPO

A traditional description of the OPO is obtained by exploiting the input–output formalism [25]. As depicted in the top panel of Fig. 1, the dynamics of the OPO are characterized by the input and output modes $a_{\text{in/out}}^{\text{ic/oc}}$ associated with the input and output coupler, the input modes associated with the crystal losses $a^{\text{cr},1/\text{cr},2}$, and the coherent evolution of the cavity mode a_{cav} generated by the squeezing Hamiltonian $H_s = i\frac{1}{2}g(a_{\text{cav}}^{\dagger 2} - a_{\text{cav}}^2)$, where we have assumed to fix the laser pump in order to amplify the quadrature $q = (a_{\text{cav}} + a_{\text{cav}}^{\dagger})/\sqrt{2}$ of the field inside the cavity. The input–output operators satisfy the canonical commutation relations (CCR) $[a_{\text{in/out}}^{\text{ic/oc}}, a_{\text{in/out}}^{\text{ic/oc}\dagger}] = [a^{\text{cr},1/\text{cr},2}, a^{\text{cr},1/\text{cr},2\dagger}] = 1$, while the cavity mode evolves such that $[a_{\text{cav}}(t), a_{\text{cav}}^{\dagger}(t')] = \delta(t - t')$ [25]. We now introduce the parameters η_{in} and η_{esc} and the squeezing parameter d . The input and output parameters depend on the loss rates at both the input coupler (γ_{ic}) and the output coupler (γ_{oc}) and the rate of internal losses of the crystal (γ_{cr}); see Fig. 1. We have

$$\eta_{\text{in}} = \gamma_{\text{ic}}/\gamma, \quad \eta_{\text{esc}} = \gamma_{\text{oc}}/\gamma, \quad (1)$$

where $\gamma = \gamma_{\text{ic}} + \gamma_{\text{oc}} + 2\gamma_{\text{cr}}$. The squeezing parameter d is proportional to the coupling of the squeezing Hamiltonian and reads $d = g/\gamma$, and the stability condition of the OPO imposes $d < 1$ [25].

By considering a roundtrip of the cavity of duration τ , defining $\tilde{a}_{\text{cav}} = \sqrt{\tau}a_{\text{cav}}$, and in the presence of high-reflectivity mirrors, the Langevin equation for the cavity mode and its boundary condition reads [25]

$$\begin{aligned} \frac{d\tilde{a}_{\text{cav}}}{dt} = & g\tilde{a}_{\text{cav}}^{\dagger}(t) - \gamma\tilde{a}_{\text{cav}}(t) + \sqrt{2\gamma_{\text{ic}}}a_{\text{in}}^{\text{ic}} \\ & + \sqrt{2\gamma_{\text{oc}}}a_{\text{in}}^{\text{oc}} + \sqrt{2\gamma_{\text{cr}}}(a^{\text{cr},1} + a^{\text{cr},2}), \end{aligned} \quad (2a)$$

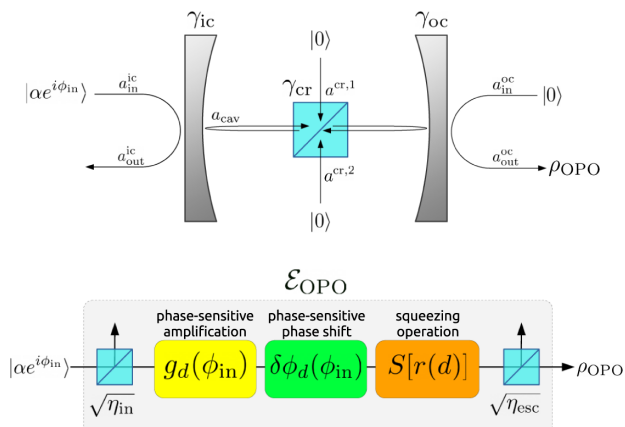


Fig. 1. Top: schematic diagram of an OPO in the input–output description with a coherent state $|\alpha e^{i\phi_{\text{in}}}\rangle$ entering the input coupler. Bottom: block scheme. The dynamics of the OPO can be described as the subsequent application of phase-sensitive amplification $g_d(\phi_{\text{in}})$, phase-sensitive phase shift $\delta\phi_d(\phi_{\text{in}})$, and squeezing $S[r(d)]$.

$$a_{\text{out}}^{\text{ic/oc}} = -a_{\text{in}}^{\text{ic/oc}} + \sqrt{2\gamma_{\text{ic/oc}}}\tilde{a}_{\text{cav}}. \quad (2b)$$

Considering the device in the stationary regime, Eq. (2) can be exploited to express the output mode in function of the input ones as

$$\begin{aligned} a_{\text{out}}^{\text{oc}} = & d(a_{\text{out}}^{\text{oc}\dagger} + a_{\text{in}}^{\text{oc}\dagger}) + (\eta_{\text{esc}} - \eta_{\text{in}} - 2\eta_{\text{cr}})a_{\text{in}}^{\text{oc}} \\ & + 2\sqrt{\eta_{\text{in}}\eta_{\text{esc}}}a_{\text{in}}^{\text{ic}} + 2\sqrt{\eta_{\text{cr}}\eta_{\text{esc}}}(a^{\text{cr},1} + a^{\text{cr},2}), \end{aligned} \quad (3)$$

with $\eta_{\text{cr}} = \gamma_{\text{cr}}/\gamma$. The last equation is not in closed form; therefore, it is convenient to pass to quadratures

$$q_{\text{out}} = \frac{a_{\text{out}}^{\text{oc}} + a_{\text{out}}^{\text{oc}\dagger}}{\sqrt{2}}, \quad p_{\text{out}} = \frac{a_{\text{out}}^{\text{oc}} - a_{\text{out}}^{\text{oc}\dagger}}{\sqrt{2}i}. \quad (4)$$

For an initial coherent state at the input coupler $|\alpha e^{i\phi_{\text{in}}}\rangle$, $\alpha \in \mathbb{R}_+$, and the vacuum in all other ports, the final state at the output coupler ρ_{OPO} is such that

$$\{\langle q_{\text{out}} \rangle, \langle p_{\text{out}} \rangle\} = \sqrt{2}\{\tilde{\alpha}_q \cos \phi_{\text{in}}, \tilde{\alpha}_p \sin \phi_{\text{in}}\}, \quad (5a)$$

$$\text{Var}[q_{\text{out}}] = \frac{1}{2} \left[1 + \eta_{\text{esc}} \frac{4d}{(1-d)^2} \right] \equiv \Sigma_q^2, \quad (5b)$$

$$\text{Var}[p_{\text{out}}] = \frac{1}{2} \left[1 - \eta_{\text{esc}} \frac{4d}{(1+d)^2} \right] \equiv \Sigma_p^2, \quad (5c)$$

with

$$\tilde{\alpha}_q = 2\frac{\sqrt{\eta_{\text{in}}\eta_{\text{esc}}}\alpha}{1-d}, \quad \tilde{\alpha}_p = 2\frac{\sqrt{\eta_{\text{in}}\eta_{\text{esc}}}\alpha}{1+d}. \quad (6)$$

In Eq. (5c), we clearly have $\Sigma_p^2 < 1/2$, showing squeezing in the p_{out} quadrature. Moreover, two other effects induced by the OPO are a phase-sensitive amplification and a phase-sensitive phase shift. By computing expectation values on Eq. (3) with the same input states, we get

$$\langle a_{\text{out}}^{\text{oc}} \rangle = 2\sqrt{\eta_{\text{in}}\eta_{\text{esc}}}\alpha_{\text{out}} e^{i\phi_{\text{out}}}, \quad (7)$$

where

$$\alpha_{\text{out}} = \frac{\alpha\sqrt{1 + 2d \cos(2\phi_{\text{in}}) + d^2}}{1-d^2}, \quad (8a)$$

$$\tan \phi_{\text{out}} = \frac{1+d}{1-d} \tan \phi_{\text{in}}. \quad (8b)$$

An equivalent description of the OPO may be obtained working in the Schrödinger picture through the block scheme sketched in the bottom panel of Fig. 1. We consider a single mode of radiation a entering the OPO, $[a, a^\dagger] = 1$. Then, the block scheme consists of the sequential application of unitary operations associated with all of the transformations produced by the OPO, that is beam splitters of transmissivity $\eta_{\text{in/esc}}$ for the input and output couplers, respectively, phase-sensitive amplification $g_d(\phi_{\text{in}})$, phase-sensitive phase shift $\delta\phi_d(\phi_{\text{in}})$, and squeezing $S[r(d)] = \exp\{\frac{1}{2}r(d)[a^{\dagger 2} - a^2]\}$. In order to obtain an output state with the expectations given in Eq. (5), we should set

$$g_d(\phi_{\text{in}}) = 2\frac{\sqrt{1 - 2d \cos(2\phi_{\text{in}}) + d^2}}{1-d^2}, \quad (9a)$$

$$\delta\phi_d(\phi_{in}) = \arctan\left(\frac{1+d}{1-d}\tan\phi_{in}\right) - \phi_{in}, \quad (9b)$$

$$\exp[r(d)] = \frac{1+d}{1-d}. \quad (9c)$$

The block scheme defines a quantum completely positive (CP) map \mathcal{E}_{OPO} such that $\mathcal{E}_{\text{OPO}}(|\alpha e^{i\phi_{in}}\rangle\langle\alpha e^{i\phi_{in}}|) = \rho_{\text{OPO}}$, and this approach proves to be equivalent to the input–output one. Moreover, since the block scheme involves the subsequent application of unitary operations associated with linear or bilinear Hamiltonians [26], we conclude that ρ_{OPO} is a Gaussian state, and \mathcal{E}_{OPO} is a Gaussian CP map. Therefore, prime and second moments suffice for a full description of the output state.

3. CASE I: PHASE MEASUREMENT USING A NOISY PROBE

Let us now address case I of Fig. 2. We consider as a probe of a coherent state $\rho_0 = |\alpha\rangle\langle\alpha|$, $\alpha \in \mathbb{R}_+$, assuming, without loss of generality, the average value of its phase to be fixed. Indeed, it is typically possible to control the average phase by employing a suitable feedback protocol [18,27]. The coherent seed undergoes phase noise (Fig. 2) whose overall effect is the application of a random phase shift is Gaussian distributed [14,23,24]. That is

$$\rho_D = \mathcal{E}_\sigma(|\alpha\rangle\langle\alpha|) = \int_{\mathbb{R}} d\psi \frac{e^{-\psi^2/(2\sigma^2)}}{\sqrt{2\pi\sigma^2}} U_\psi |\alpha\rangle\langle\alpha| U_\psi^\dagger, \quad (10)$$

where $U_\psi = e^{-i\psi a^\dagger a}$ is a phase shift operation, and σ is the amplitude of the noise. Then, following case I of Fig. 2, we let the dephased state pass through an OPO, described by the map \mathcal{E}_{OPO} , obtaining the final state $\rho_{\text{out}} = \mathcal{E}_{\text{OPO}}(\mathcal{E}_\sigma(|\alpha\rangle\langle\alpha|))$. The task is to find a feasible strategy to measure the optical phase and to state whether the OPO is able to compensate the effects of phase noise by comparing the results obtained with states ρ_D and ρ_{out} .

Figure 3 shows the effects of such transformations at the level of quantum states. In the phase space, dephasing causes an inhomogeneous spread of the coherent state, which makes state ρ_D not Gaussian anymore. Then, the action of the OPO squeezes quadrature p at the expense of magnifying the variance of q .

To give an estimate of the phases of ρ_D and ρ_{out} and to assess whether the OPO can *squeeze* the noise, we will consider two different approaches. First of all, we perform a *direct measurement* of the phase, exploiting a phase positive operator-valued measure (POVM). Then, we present an *indirect measurement* procedure based on post processing of the data of two separate

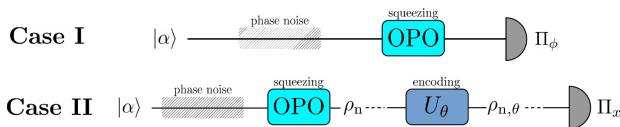


Fig. 2. Schematic diagram of the two scenarios discussed in this paper.

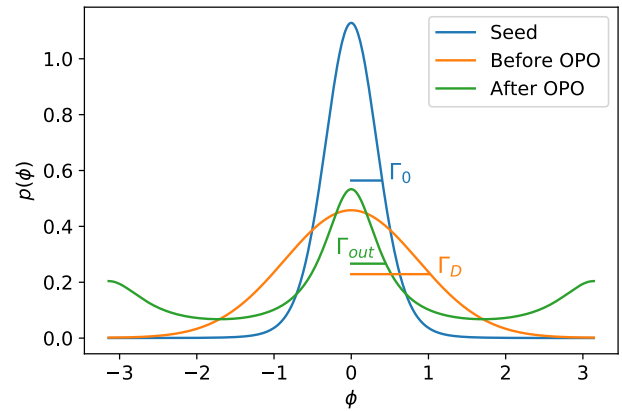
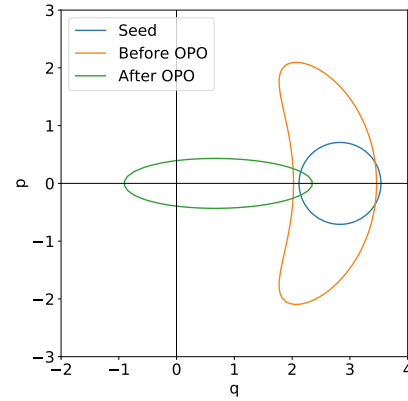


Fig. 3. Top: phase space representation of ρ_0 , ρ_D , and ρ_{out} , where we plot the level curves at the level of the standard deviation. Bottom: phase distributions $\rho_0(\phi)$, $\rho_D(\phi)$, and $\rho_{\text{out}}(\phi)$. We set $\alpha = 2$, $\sigma = \pi/4$, and $d = 0.4$, and we used the realistic parameters $\eta_{\text{in}} = 0.01$, $\eta_{\text{esc}} = 0.93$.

homodyne detections, which will prove to give the same *qualitative* results in the regime of $\alpha \gg 1$. Actually, given this scenario, we have a priori information that the value of the phase is zero. However, the purpose of both strategies is not the estimation of the phase value, but rather to state whether or not the OPO is able to reduce a proper figure of merit representing the phase uncertainty. Furthermore, we want to underline that the goal of this section is not to make a direct comparison between the two measurements proposed. The basic idea is to show that a realistic OPO may be a convenient resource to mitigate the noise, and that this convenience is guaranteed with different phase measurement strategies employed.

A. Direct Measurement of the Phase

A convenient way to perform phase measurement is to employ a genuine phase POVM [9,10,28]. Among all possible choices, here, we consider a feasible POVM, implemented through a heterodyne detection, namely,

$$\Pi_\phi = \frac{1}{\pi} \int_0^\infty d\zeta \zeta |\zeta e^{i\phi}\rangle\langle\zeta e^{i\phi}|, \quad (11)$$

where $|\zeta e^{i\phi}\rangle$ is a coherent state. The corresponding phase probability for a given state ρ reads

$$p(\phi) = \text{Tr}[\rho \Pi_\phi], \quad (12)$$

$$= \int_0^\infty d\zeta \zeta Q[\rho](\zeta e^{i\phi}), \quad (13)$$

that is the marginal in phase of the Husimi Q -function $Q[\rho](z) = \langle z|\rho|z\rangle/\pi$, $z \in \mathbb{C}$.

Within this scenario, we have to compare the probabilities $p_0(\phi)$, $p_D(\phi)$, and $p_{\text{out}}(\phi)$ associated with the initial state ρ_0 , the dephased state ρ_D , and the output state ρ_{out} , respectively, and we have to assess in which conditions the OPO leads to a reduction of the width of the distribution. Figure 3 shows the three phase distributions. Compared to the input probability density, dephasing broadens the distribution, while squeezing introduces two secondary peaks at $\pm\pi$: a border effect caused by the π periodicity of the squeezing phase. Because of this latter effect, the proper figure of merit for the phase uncertainty shall be the half-width at half-maximum (HWHM) of the central peak.

Numerical evaluation of $p(\phi)$ in different regimes allows us to understand the role of the different parameters. We fix the OPO parameters d , η_{in} , η_{esc} considering realistic values [23] and consider several values for α and σ . Then, we compute and compare the HWHMs of the dephased distribution $\Gamma_D(\alpha, \sigma)$ and of the squeezed one $\Gamma_{\text{out}}(\alpha, \sigma, d, \eta_{\text{in}}, \eta_{\text{esc}})$. As shown in Fig. 4, if the coherent signal α is small enough, Γ_{out} is constantly inferior to Γ_D , therefore the OPO proves to be always helpful regardless the values of σ . The reason is that even with zero noise, $\sigma = 0$, there exists a regime where the squeezed HWHM $\Gamma_S(\alpha, d, \eta_{\text{in}}, \eta_{\text{esc}}) = \Gamma_{\text{out}}(\alpha, \sigma = 0, d, \eta_{\text{in}}, \eta_{\text{esc}})$ is smaller than the HWHM of the seed probability distribution $\Gamma_0(\alpha)$, since for small α the border peaks of the squeezed distribution centered in $\pm\pi$ induce a non-negligible reduction of the width of the central peak centered in zero. As a consequence, there exists a threshold coherent amplitude $\alpha_{\text{th}}(d, \eta_{\text{in}}, \eta_{\text{esc}})$, such that if $\alpha < \alpha_{\text{th}}(d, \eta_{\text{in}}, \eta_{\text{esc}})$ the OPO is always useful. The threshold is obtained by imposing the equality $\Gamma_0(\alpha_{\text{th}}) = \Gamma_S(\alpha_{\text{th}}, d, \eta_{\text{in}}, \eta_{\text{esc}})$. On the contrary, if $\alpha > \alpha_{\text{th}}(d, \eta_{\text{in}}, \eta_{\text{esc}})$, we observe a σ dependency. For small noise σ , we have $\Gamma_{\text{out}} > \Gamma_D$, and so the OPO is revealed to be useless, but, on the contrary for large noise σ , the situation is reversed and $\Gamma_{\text{out}} < \Gamma_D$. There exists a threshold noise $\sigma_{\text{th}}(\alpha, d, \eta_{\text{in}}, \eta_{\text{esc}})$ such that the OPO stays useful only for $\sigma > \sigma_{\text{th}}(\alpha, d, \eta_{\text{in}}, \eta_{\text{esc}})$. Formally, such threshold noise is obtained by imposing $\Gamma_D(\alpha, \sigma_{\text{th}}) = \Gamma_{\text{out}}(\alpha, \sigma_{\text{th}}, d, \eta_{\text{in}}, \eta_{\text{esc}})$.

B. Indirect Measurement of the Phase

The second possible method involves two different and independent homodyne measurements of q and p to avoid the unavoidable excess noise induced by joint measurements. The value of the phase is then obtained as [23]

$$\hat{\varphi} = \arctan \frac{\langle p \rangle}{\langle q \rangle}. \quad (14)$$

The exploitation of average values guarantees that squeezing border effects are absent, and we choose the variance of $\hat{\varphi}$ as a good figure of merit. By exploiting the variance propagation law, we have

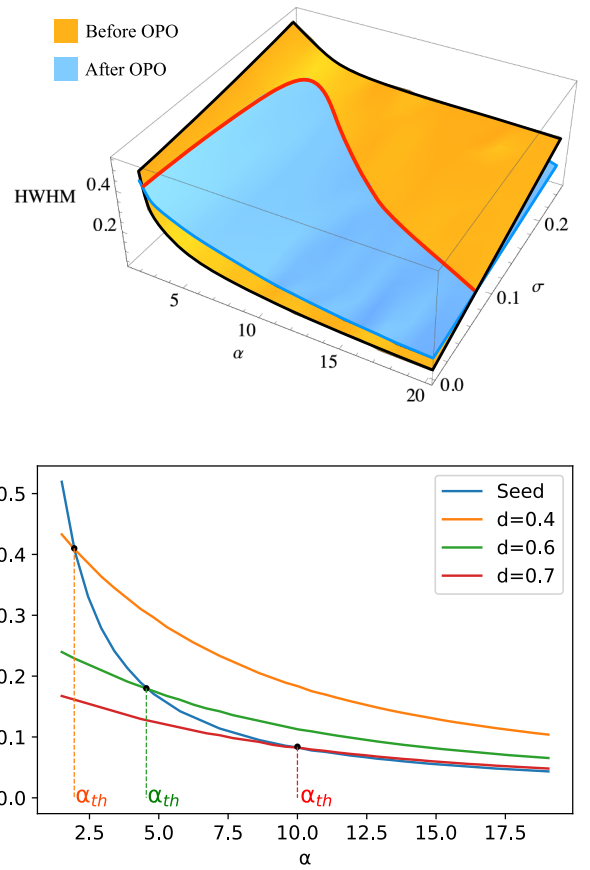


Fig. 4. Top: 3D plot of the dephased HWHM Γ_D and the squeezed HWHM Γ_{out} as function of α and σ , with $d = 0.4$. There exists a threshold signal α_{th} such that for smaller α , $\Gamma_{\text{out}} < \Gamma_D$ for all σ , while for larger α the intersection between the two surfaces identifies the threshold noise σ_{th} . Bottom: plot of the HWHMs Γ_0 of the seed and Γ_S for different values of d as functions of α in the absence of noise ($\sigma = 0$). The intersection between Γ_0 and Γ_S defines the threshold α_{th} , which appears to be an increasing function of d . We used the realistic parameters $\eta_{\text{in}} = 0.01$, $\eta_{\text{esc}} = 0.93$.

$$\Delta^2 \varphi = \frac{\langle q \rangle^2 \Delta^2 p + \langle p \rangle^2 \Delta^2 q}{(\langle q \rangle^2 + \langle p \rangle^2)^2}. \quad (15)$$

The input state ρ_0 is Gaussian with

$$\langle q \rangle_0 = \sqrt{2}\alpha, \quad \langle p \rangle_0 = 0, \quad \Delta^2 q_0 = \Delta^2 p_0 = 1/2, \quad (16)$$

therefore, $\Delta^2 \varphi_0 = 1/4\alpha^2$. For the dephased state ρ_D , we have

$$\langle q \rangle_D = e^{-\sigma^2/2} \sqrt{2}\alpha, \quad \langle p \rangle_D = 0, \quad (17)$$

and

$$\Delta^2 q_D = \frac{1}{2} + \alpha^2 (1 - e^{-\sigma^2})^2, \quad \Delta^2 p_D = \frac{1}{2} + \alpha^2 (1 - e^{-2\sigma^2}), \quad (18)$$

leading to

$$\Delta^2 \varphi_D = \frac{e^{\sigma^2}}{4\alpha^2} + \sinh^2 \sigma^2 > \Delta^2 \varphi_0. \quad (19)$$

Finally, the squeezed dephased state ρ_{out} has

$$\langle q \rangle_{\text{out}} = e^{-\sigma^2/2} \sqrt{2\tilde{\alpha}_q}, \quad \langle p \rangle_{\text{out}} = 0, \quad (20)$$

and

$$\Delta^2 q_{\text{out}} = \Sigma_q^2 + \tilde{\alpha}_q^2 (1 - e^{-\sigma^2}), \quad \Delta^2 p_{\text{out}} = \Sigma_p^2 + \tilde{\alpha}_p^2 (1 - e^{-2\sigma^2}), \quad (21)$$

thereafter, we obtain

$$\Delta^2 \varphi_{\text{out}} = \frac{e^{\sigma^2}}{2\tilde{\alpha}_q^2} \Sigma_p^2 + \frac{\tilde{\alpha}_p^2}{\tilde{\alpha}_q^2} \sinh \sigma^2. \quad (22)$$

The variance of $\hat{\varphi}$ is given by two contributions, the former is correlated to the signal-to-noise ratio $\Delta^2 p / \langle q \rangle^2$ of the noiseless state ρ_0 , the latter is a pure excess noise term. The excess noise term is always reduced after the OPO since $\tilde{\alpha}_p / \tilde{\alpha}_q < 1$. On the contrary, the signal-to-noise term after the OPO turns out to be lower than before only if $\Sigma_p^2 / \tilde{\alpha}_q^2 < 1/2\alpha^2$. This latter condition defines a threshold squeezing d_{th} at fixed values of η_{in} and η_{esc} via the equation

$$f(d_{\text{th}}) \equiv \frac{4\eta_{\text{in}}\eta_{\text{esc}}}{(1-d_{\text{th}})^2} \left[1 + \frac{d_{\text{th}}}{\eta_{\text{in}}} e^{-2r(d_{\text{th}})} \right] - 1 = 0, \quad (23)$$

where $r(d)$ is defined in Eq. (9c). If $d > d_{\text{th}}(\eta_{\text{in}}, \eta_{\text{esc}})$, the OPO proves always useful, otherwise, if $d < d_{\text{th}}(\eta_{\text{in}}, \eta_{\text{esc}})$, the OPO amplifies the signal-to-noise ratio on quadratures but reduces the excess noise. For small σ , it is the signal-to-noise term to dominate, therefore the OPO is useless. When σ is large, the situation is reversed. There is a trade-off between the two contributions leading to the existence of a threshold noise σ_{th} , above which squeezing shows a benefit. The threshold condition leads to

$$\sigma_{\text{th}}^2 = \frac{1}{2} \ln \left[\frac{2\alpha^2(\tilde{\alpha}_q^2 - \tilde{\alpha}_p^2)}{\tilde{\alpha}_q^2 + 2\alpha^2(\tilde{\alpha}_q^2 - \tilde{\alpha}_p^2 - \Sigma_p^2)} \right], \quad (24)$$

and it agrees, at least qualitatively, to that obtained with a genuine phase measurement in the regime $\alpha \gg 1$ (see Fig. 4). We notice that this agreement is only *qualitative*, since the two strategies presented here cannot be directly compared because they require a different number of measurements. In order to make a direct comparison between them, one has to decrease α by a factor $1/\sqrt{2}$ in the indirect case to compensate the fact that two distinct measurements are performed on two copies of the state. Beside it all, the agreement between the two strategies also provides a validation for the post-processing method of Section 3.B, which itself represents a convenient practical choice for experiments [23].

4. CASE II: ESTIMATION OF A PHASE SHIFT USING A NOISY PROBE

The second scenario, in which we discuss the exploitation of an OPO, is related to the estimation of a phase shift applied to a noisy probe. In particular, we analyze the protocol depicted in Fig. 2, case II within the framework of quantum estimation theory (see Appendix A). We consider as the probe the state

$$\rho_n = \mathcal{E}_{\text{OPO}}(\mathcal{E}_\sigma(|\alpha\rangle\langle\alpha|)), \quad (25)$$

on which we encode a phase shift θ through the unitary $U_\theta = e^{-i\theta a^\dagger a}$. After the encoding stage, the quantum state of radiation is sent into a channel until it reaches a receiver that performs measurements. In this case, the task is to decide the optimal POVM $\{\Pi_x\}$ to infer the value of θ . Here, we decide to restrict to a subclass of feasible measurements, i.e., *homodyne measurements*. We investigate how the exploitation of the OPO modifies the quantum Fisher information (QFI) H and the Fisher information (FI) F of a homodyne detection of $x_\phi = \cos \phi q + \sin \phi p$. By comparing the two of them, we decide whether homodyne measurements can be optimal and, in particular, which is the best quadrature $x_{\phi_{\text{max}}}$ that maximizes the FI. In the following, first of all, we analyze the case in absence of phase diffusion as a benchmark, and, secondly, we discuss the noisy case.

A. Noiseless Estimation Scheme

In the absence of phase noise (but with the OPO still present), the probe state of the protocol in Fig. 2, case II is the state ρ_{OPO} derived in Section 2. Then, the encoded state reads

$$\rho_{\text{nl},\theta} = U_\theta \rho_{\text{OPO}} U_\theta^\dagger. \quad (26)$$

ρ_{OPO} is a Gaussian state with prime moments $\mathbf{R}_{\text{OPO}} \equiv \langle \hat{\mathbf{r}} \rangle = (\sqrt{2\tilde{\alpha}_q}, 0)$ and covariance $\sigma_{\text{OPO}} \equiv \langle \{(\hat{\mathbf{r}} - \mathbf{R}_{\text{OPO}}), (\hat{\mathbf{r}} - \mathbf{R}_{\text{OPO}})^T\} \rangle / 2 = \text{Diag}[\Sigma_q^2, \Sigma_p^2]$, $\hat{\mathbf{r}} = (q, p)$. Therefore, the statistical model $\rho_{\text{nl},\theta}$ is still Gaussian with prime moments $\mathbf{R}_\theta = \mathcal{R}_\theta \mathbf{R}_{\text{OPO}}$ and covariance $\sigma_\theta = \mathcal{R}_\theta \sigma_{\text{OPO}} \mathcal{R}_\theta^T$, where \mathcal{R}_θ is the rotation matrix

$$\mathcal{R}_\theta = \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix}. \quad (27)$$

In general, for a generic Gaussian state ρ_λ with prime moments \mathbf{R}_λ and covariance σ_λ , the QFI has the following analytical expression:

$$H(\lambda) = \frac{1}{2} \frac{\text{Tr}[(\sigma_\lambda^{-1} \sigma'_\lambda)^2]}{1 + \mu_\lambda^2} + 2 \frac{\mu_\lambda'^2}{1 - \mu_\lambda^4} + \mathbf{R}'_\lambda{}^T \sigma_\lambda^{-1} \mathbf{R}'_\lambda, \quad (28)$$

where $A' = \partial_\lambda A$, and $\mu_\lambda = (2\sqrt{\det \sigma_\lambda})^{-1}$ is the purity of the Gaussian state ρ_λ [29–32].

In the very case examined, Eq. (34) leads to

$$H_{\text{nl}} = 4 \frac{(\Sigma_q^2 - \Sigma_p^2)^2}{1 + 4\Sigma_p^2 \Sigma_q^2} + 2 \frac{\tilde{\alpha}_q^2}{\Sigma_p^2}, \quad (29)$$

which is independent of θ . The QFI depends on both α and d . However, the α dependence is only polynomial, and so it is less relevant than the squeezing one. Therefore, in the following, we keep α fixed and study the QFI dependence on the squeezing factor $r = \ln[(1+d)/(1-d)]$. As depicted in Fig. 5, the QFI is a growing function on r . Thus, the most sensitive probe is obtained for $r \gg 1$, i.e., $d \approx 1$. It is also worth finding out the asymptotic scaling of the QFI by evaluating its dependence on the energy,

$$N = \text{Tr}[\rho_{\text{nl},\theta} a^\dagger a] = \frac{\Sigma_q^2 + \Sigma_p^2 + \tilde{\alpha}_q^2 - 1}{2}, \quad (30)$$

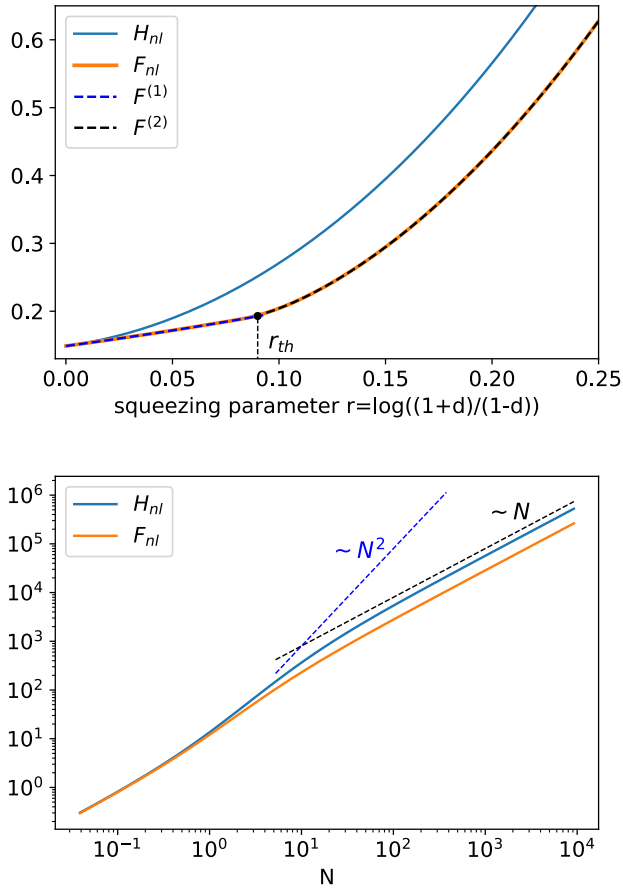


Fig. 5. Top: QFI and optimized FI as a function of r for $\alpha = 1$. For $r \geq r_{th}(\alpha, \eta_{in}, \eta_{esc})$, the optimized quadrature is $\phi^{(2)}$, and F_{nl} coincides with $F^{(2)}$, whereas if $r < r_{th}(\alpha, \eta_{in}, \eta_{esc})$ F_{nl} is equal to $F^{(1)}$ (see the text for details). Bottom: QFI and optimized FI as a function of N for $\alpha = 0.2$ (plot in log scale). The dashed lines refer to the Heisenberg scaling $\sim N^2$ and shot-noise one $\sim N$. We used the realistic parameters $\eta_{in} = 0.01, \eta_{esc} = 0.93$.

by keeping α fixed and varying only d . Eventually, the QFI H_{nl} shows shot noise scaling,

$$H_{nl} \approx \frac{4}{1 - \eta_{esc}} \frac{1 + 4\eta_{in}\alpha^2}{1 + 2\eta_{in}\alpha^2} N, \quad (31)$$

whose origin can be addressed to the non-negligible losses characterizing the OPO dynamics.

In regards to the analysis of the FI, it is helpful to write the probe state ρ_{OPO} in the form of a displayed squeezed thermal state [26,33],

$$\rho_{OPO} = D(\beta) S(\xi) \nu^{th}(\bar{n}) S(\xi)^\dagger D(\beta)^\dagger, \quad (32)$$

where $D(\beta) = \exp(\beta a^\dagger - \beta^* a)$ is the displacement operator, $S(\xi) = \exp[\frac{1}{2}\xi(a^{\dagger 2} - a^2)]$ is the squeezing operator, and $\nu^{th}(\bar{n}) = \bar{n}^{a^\dagger a} / (\bar{n} + 1)^{a^\dagger a + 1}$ is a thermal state with mean number of photons \bar{n} . For the state ρ_{OPO} , the values of the parameters are $\beta = \tilde{\alpha}_q$, $\exp(2\xi) = \sqrt{\Sigma_q^2 / \Sigma_p^2}$, and $(1 + 2\bar{n})^2 = 4\Sigma_q^2 \Sigma_p^2$.

Actually, it is proved that for a displayed squeezed thermal state the optimal measurement is not Gaussian [34], and no homodyne can exactly reach the QFI. Nevertheless, it is still

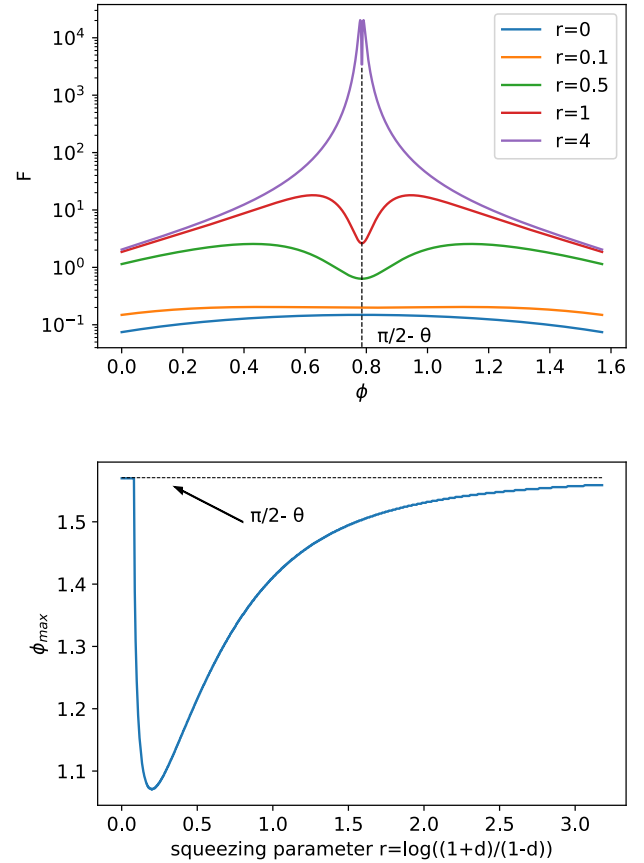


Fig. 6. Top: FI of the measurement of x_ϕ as a function of ϕ for different values of the squeezing parameter r . Bottom: optimized quadrature ϕ_{max} as a function of r . We set $\alpha = 1$, and we used the realistic parameters $\eta_{in} = 0.01, \eta_{esc} = 0.93$.

worth it to construct an optimized homodyne measurement since it becomes nearly optimal (i.e., $FI \approx QFI$) in the best working regime $r \gg 1$.

To construct the optimized homodyne, we again keep α fixed and let only the squeezing parameter r vary. For every r , we compute the FI associated with $x_\phi = \cos \phi q + \sin \phi p$ as a function of ϕ and find the value ϕ_{max} maximizing it, as depicted in Fig. 6. In the end, the optimized FI F_{nl} , displayed in Fig. 5, turns out to be a piecewise-defined function, since two quadrature candidates exist for the choice of ϕ_{max} [34]:

1. $\phi^{(1)} = \pi/2 - \theta$, whose corresponding FI is

$$F^{(1)} = \frac{2\tilde{\alpha}_q^2}{\Sigma_p^2}, \quad (33)$$

2. $\phi^{(2)} = \pi/2 - \theta - \chi/2$, where χ satisfies

$$\cos \chi = \frac{(\Sigma_q^2 - \Sigma_p^2)^3 + \Sigma_q^2 \tilde{\alpha}_q^2 (\Sigma_q^2 + \Sigma_p^2)}{(\Sigma_q^2 + \Sigma_p^2)(\Sigma_q^2 - \Sigma_p^2)^2 + \Sigma_q^2 \tilde{\alpha}_q^2 (\Sigma_q^2 - \Sigma_p^2)} \quad (d \neq 0), \quad (34)$$

for which the corresponding value of the FI reads

$$F^{(2)} = \frac{[(\Sigma_q^2 - \Sigma_p^2)^2 + \Sigma_q^2 \tilde{\alpha}_q^2]^2}{2\Sigma_q^2 \Sigma_p^2 (\Sigma_q^2 - \Sigma_p^2)^2}. \quad (35)$$

The second measurement is well defined only if $|\cos \chi| \leq 1$, namely,

$$\tilde{\alpha}_q \leq (\Sigma_q^2 - \Sigma_p^2) / \sqrt{\Sigma_q^2}, \quad (36)$$

providing a threshold squeezing $r_{\text{th}}(\alpha, \eta_{\text{in}}, \eta_{\text{esc}})$, such that for smaller r the function $F^{(2)}$ has no physical meaning, and the optimized quadrature is $\phi^{(1)}$, while for larger r , the homodyne measurement of quadrature $\phi^{(2)}$ is well defined, and the optimized quadrature becomes $\phi^{(2)}$. The physical explanation of such behavior becomes clear by observing the ϕ dependence of the FI displayed in Fig. 6. For small r , the function has a single maximum at $\pi/2 - \theta$, but, for larger r , the maximum splits into two symmetric peaks, and $\pi/2 - \theta$ turns into a local minimum. Then, by increasing r further, the position of the peaks asymptotically converges to $\pi/2 - \theta$. Regarding the energy scaling of F_{nl} , by rearranging Eq. (35), we again get shot noise scaling,

$$F_{\text{nl}} \approx 2 \frac{1 + 2\eta_{\text{in}}\alpha^2}{1 - \eta_{\text{esc}}} N. \quad (37)$$

B. Noisy Estimation Scheme

If phase noise is present, the statistical model reads

$$\rho_{n,\theta} = U_\theta \rho_n U_\theta^\dagger, \quad (38)$$

where ρ_n is still given in Eq. (25). The presence of this kind of noise prevents us from obtaining analytical solutions. Therefore, we keep the results of Section 4.A as a benchmark and consider how the noise affects a specific case. We perform a homodyne of $x_{\phi_{\text{max}}}$, where ϕ_{max} is the optimized quadrature of Fig. 6. For several values of σ , we analyze the dependence of the FI,

$$F_n = \int dx \frac{[\partial_\theta p(x|\theta)]^2}{p(x|\theta)}, \quad p(x|\theta) = \text{Tr}[\rho_{n,\theta} x_{\phi_{\text{max}}}], \quad (39)$$

on the energy N of Eq. (30). Moreover, to compare the noiseless and noisy cases, we introduce the relative fluctuations parameter

$$\epsilon = \frac{|F_n - F_{\text{nl}}|}{F_{\text{nl}}}. \quad (40)$$

The numerical results of ϵ , depicted in Fig. 7, show that the exploitation of the OPO is able to compensate almost completely the detriments of phase noise. In particular, using an OPO is crucial to maintain the shot noise regime for all values of σ . Otherwise, if we consider the protocol of Fig. 2, case II without the OPO, an upper bound exists for the QFI [35], namely,

$$H_{\text{without OPO}} \leq H_{\text{UB}} = \frac{4N}{1 + 4N\sigma^2}, \quad (41)$$

saturating for large N to the value $1/\sigma^2$.

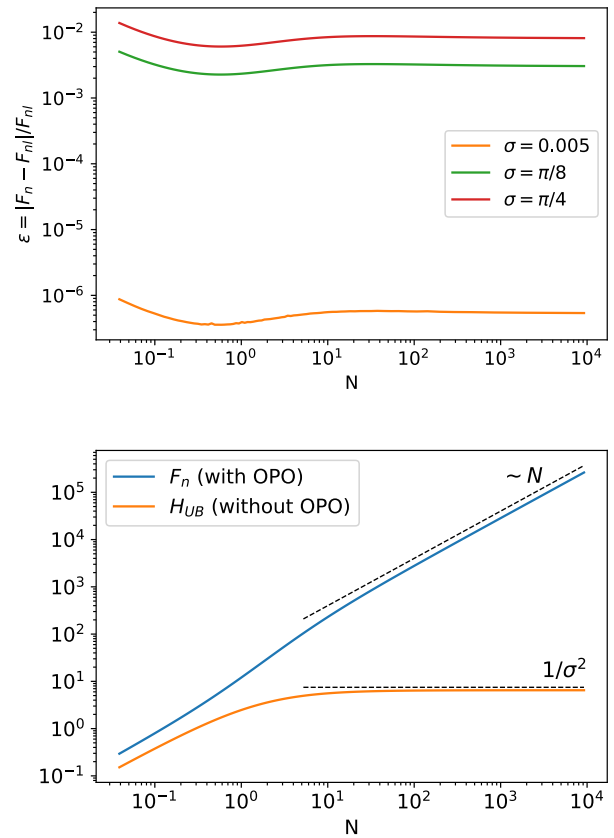


Fig. 7. Top: relative fluctuations given in Eq. (46) as a function of N for different values of the noise parameter σ . Bottom: plot of the F_n and H_{UB} as functions of N for $\sigma = \pi/8$. We set $\theta = 0$, $\alpha = 0.2$, and we used the realistic parameters $\eta_{\text{in}} = 0.01$, $\eta_{\text{esc}} = 0.93$.

5. CONCLUSIONS

In summary, we have studied several scenarios where phase noise prevents the use of optical phase as a degree of freedom for quantum information tasks and discussed whether an OPO may be employed to mitigate, or even compensate, the effects of noise. Such a method could be interesting with the intent of reducing the noise of the laser in a regime of high frequency.

Firstly, we have developed a block-diagram model to describe an OPO in the form of a subsequent application of Gaussian operations: beam splitters, phase-sensitive amplification, phase-sensitive phase shift, and squeezing. Such a description in the Schrödinger picture allows us to give an explicit expression for the output state of radiation. Indeed, given an initial coherent state, the output state is a Gaussian state with well-defined prime moments and covariance.

With the new description of the OPO, we have addressed the first case under investigation: the measurement of the phase of a quantum state of radiation. We have introduced two possible approaches. A first standard approach involves the introduction of a phase POVM (implemented through heterodyne detection). It leads to the conclusion that the OPO reduces phase noise, i.e., the width of the probability distribution associated with the POVM, for small signal amplitude or large signal amplitude and large dephasing. The second approach consists of a post-processing method based on the outcomes of two distinct

homodyne detections and brings the same phenomenology as before in the regime of large coherent amplitudes. In both cases, according to the value of parameters α , σ , d , there exists a regime where the procedure gives a phase outcome with a larger uncertainty than the one of the initial coherent state and another regime in which the uncertainty is smaller. This leads to the conclusion that in such a regime the OPO is able to *fully*, or at least *partially*, compensate the noise.

The second scenario discussed has been an estimation scheme based on the encoding of a phase shift θ on the probe state. We have considered a dephased coherent state passed through an OPO as the probe state and searched for the optimal POVM to detect θ within the subclass of homodyne measurements. We have studied in detail the noiseless protocol, obtaining the optimized quadrature ϕ_{\max} that allows us to infer θ with negligible uncertainty. Passing to the noisy case, such a situation is still maintained. The noise weakly affects the FI, and shot noise scaling, i.e., the proper scaling of the input coherent state, is conserved. Therefore, in such a case, the noise mitigation by the OPO is *complete* in regards to the scaling with the probe average photon number.

Our results confirm that it is possible to develop suitable OPO-based strategies to compensate phase noise with current technology and, thus, pave the way for the full exploitation of optical phase in quantum technologies.

APPENDIX A: ELEMENTS OF QUANTUM ESTIMATION THEORY

The estimation of a parameter is a frequent task in quantum mechanics, since several physical quantities cannot be directly measured. Here, we present the basic features of the theory behind it [36,37]. We consider a family of quantum states labeled by a parameter λ , $\{\rho_\lambda\}_\lambda$, usually called the *statistical model*. Usually, we perform a generalized measurement described by a POVM $\{\Pi_x\}$, obtaining a statistical sample of M outcomes $\mathbf{x} = \{x_1, \dots, x_M\}$. This sample is processed by means of a map $\hat{\lambda}(\mathbf{x})$, called an *estimator*, to infer the value of the parameter λ . The task is to find the optimal POVM that allows us to estimate the value of λ with the lowest possible uncertainty, i.e., the maximum precision. The conditional probability of the outcome x given λ is

$$p(x|\lambda) = \text{Tr}[\rho_\lambda \Pi_x]. \quad (\text{A1})$$

If the estimator is unbiased, there exists a lower bound to its variance, depending on the FI of the distribution $p(x|\lambda)$,

$$F(\lambda) = \int dx \frac{[\partial_\lambda p(x|\lambda)]^2}{p(x|\lambda)}. \quad (\text{A2})$$

The bound is the so called the *Cramér–Rao bound* and reads

$$\text{Var}[\hat{\lambda}] \geq \frac{1}{MF(\lambda)}, \quad (\text{A3})$$

where we introduced the variance $\text{Var}[\hat{\lambda}] = E[\hat{\lambda}^2] - E[\hat{\lambda}]^2$ with

$$E[\hat{\lambda}^k] = \int dx p(x|\lambda) \hat{\lambda}(x)^k, \quad k \in \mathbb{N}. \quad (\text{A4})$$

However, a stricter bound, independent of the particular measurement performed, may be obtained [38–41]. We define the symmetric logarithmic derivative (SLD) L_λ by the Ljapunov equation $2\partial_\lambda \rho_\lambda = L_\lambda \rho_\lambda + \rho_\lambda L_\lambda$ and the QFI as [37]

$$H(\lambda) = \text{Tr}[\rho_\lambda L_\lambda^2]. \quad (\text{A5})$$

The QFI leads to the quantum Cramér–Rao bound

$$\text{Var}[\hat{\lambda}] \geq \frac{1}{MH(\lambda)}. \quad (\text{A6})$$

In assessing a quantum estimation scheme, both the QFI and the FI are important tools. The QFI identifies the ultimate limits on precision allowed by quantum mechanics, independent of the measurement, while the FI fixes the minimum possible uncertainty given a particular measurement strategy, namely, a POVM. In this present work, we will address a subclass of possible measurements, that is homodyne measurements, and determine their performance by comparing the QFI and FI.

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